Isothermal DC and Microwave Characterizations of Power RF Silicon LDMOSFETs

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Abstract—Presented in this paper are two new approaches for the acquisition of both iso-thermal dc current-voltage (I–V) characteristics and microwave S-parameters of power RF LDMOSFETs. In the first approach, three-dimensional (3-D) tensor product B-spline representation is used to extract iso-thermal dc I–V characteristics from dc I–V characteristics measured at various substrate temperatures. The average device surface temperature is measured using an infrared sensor. A single effective thermal resistance is found to map the entire electrothermal profile of the device justifying the iso-thermal dc I–V definition used. In the second approach, iso-thermal I–V and microwave data are directly measured with an efficient procedure that keeps the average device surface temperature constant. Excellent agreement is obtained between the numerical extraction and the direct measurement approach. Finally, the comparison of the transconductance extracted from the iso-thermal dc I–V and microwave data confirms the presence of a small low-frequency dispersion in LDMOSFET not due to self-heating.

Index Terms—electrothermal modeling, isothermal IV characteristic, LDMOSFET, low-frequency dispersion, pulsed IV, self-heating.

I. INTRODUCTION

PACKAGED silicon power LDMOSFET transistors are finding increasing use for RF power amplifier design in medium- to high-power applications. Due to the high power which can be dissipated in these devices, of particular concern is the measurement and modeling of their electrothermal behavior [1]. For such modeling, isothermal microwave data are required to extract the FET model [2] and isothermal current-voltage (I–V) data to determine the quiescent operating point of the device in the presence of self-heating and self-biasing. Under dc operation the dc (I_{D,DC}) and isothermal (I_{D,iso}) I–V drain currents are related by

\[ I_{D,DC}(V_{GS}, V_{DS}, T_{sub}) = I_{D,iso}(V_{GS}, V_{DS}, T_{dev}) \]

\[ \text{with } T_{dev} = T_{sub} + R_{\text{th,eff}}(T_{sub}) \times P_{\text{avg}} \] (1)

where

- \( T_{sub} \): substrate temperature;
- \( T_{dev} \): average device temperature;
- \( R_{\text{th,eff}} \): effective thermal resistance;
- \( P_{\text{avg}} \): average power dissipated by the FET.

In the presence of strong self heating, such as in class B and AB amplifiers, the isothermal I–V characteristics which are a function of the device temperature must be used instead of the dc I–V characteristics which are a function of the substrate temperature only.

Note that in general pulsed I–V characteristics \( I_{D,\text{pulsed}} \) are not the same as the isothermal I–V characteristics \( I_{D,\text{iso}} \). Indeed pulsed I–V characteristics have a double bias dependence \( I_{D,\text{pulsed}}(V_{GS}, V_{DS}, T_{dev,\text{pul}}) \), as they are a function of both the instantaneous voltages \( V_{GS} \) and \( V_{DS} \) and the dc bias \( V_{GS} \) and \( V_{DS} \). To illustrate this feature, we show in Fig. 1 the measurement trajectory for the pulsed I–V characteristics which clearly identifies the dc bias point. Typically different pulsed I–V characteristics result if a different dc bias point is used. Pulsed I–V characteristics cannot therefore be equivalent to the uniquely defined isothermal I–V characteristics.

To investigate the difference between pulsed I–V and isothermal I–V curves, consider the case of SOI-MOSFETs which are known to exhibit large low-frequency dispersions (large low-frequency dependence of its small-signal parameters) resulting in notably different \( g_m \) and \( d_m \) extracted at dc and RF-microwave. The behavior of SOI-MOSFETs can be well modeled by the electrothermal model shown in Fig. 2 [4]. This model is based upon a physical topology combining a FET model and a parasitic bipolar-transistor [3], [4] with a floating base driven by the impact ionization current. The
Fig. 2. (a) Self-biasing model topology to fit both dc and RF and (b) electrical network representing the thermal network model.

Fig. 3. Comparison of isothermal $I_{D,DC}$ (dashed lines) and pulsed $I_{D,RF}$ (solid lines) $I-V$ characteristics. Both curves intercept at the dc bias-point used by the pulsed $I-V$ which is indicated by an asterisk. The isothermal $I-V$ curves feature a kink when the parasitic bipolar transistor turns on.

total FET-drain current measured is therefore the sum of the bipolar-transistor collector-current $I_C$, the impact ionization current $I_{ii}$, and the normal FET drain-current without-impact-ionization $I_{Wii}$. The parasitic bipolar-transistor which introduces part of the low-frequency dispersions in SOI-MOSFETs, performs with its long time response the seamless integration between 1) the isothermal dc $I-V$ characteristics

$$I_{D,DC}(V_{GS}, V_{DS}, T_{dev}) = I_{Wii}(V_{GS}, V_{DS}) + I_{ii}(V_{GS}, V_{DS})$$

which sets the transistor’s dc biasing and 2) the pulsed $I-V$ characteristics

$$I_{D,RF}(V_{GS}, V_{DS}, V_{DS,DC}, V_{DS,DC}, T_{dev,DC}) = I_{Wii}(V_{GS}, V_{DS}) + I_{Wii}(V_{GS}, V_{DS}, DC)$$

which are relevant to the power transistor’s response at microwave frequencies. Note that these $I-V$ curves intersect at the dc bias-point ($V_{GIS}, V_{DS}$)

$$I_{D,RF}(V_{GIS}, V_{DS}) = I_{D,DC}(V_{GIS}, V_{DS}, T_{dev}).$$

As is shown in Fig. 3 for a SOI-MOSFET, the pulsed $I-V$ curves, which are also isothermal, and the isothermal $I-V$ curves are usually different (apart from the bias-point) because the pulsed $I-V$ bypass not only self-heating but also other slow physical processes such as parasitic bipolar-transistor and trap effects which induce additional low-frequency dispersion.

In line with this discussion, we present below new methods for obtaining isothermal $I-V$ characteristics and isothermal microwave S-parameters without using pulsed measurements.

II. DC THERMAL CHARACTERIZATIONS

We have used for this entire work Motorola’s MRF 181 RF power, n-channel enhancement mode, lateral diffused MOSFET [5]. The electrothermal test system shown in Fig. 4 was used to obtain a complete dc and thermal profile of the LDMOSFET. LabWindows [6] is used to control $V_{DS}, V_{GS}$, and the substrate temperature $T_{sub}$, while measuring the resulting non-isothermal drain current $I_{D,DC}$ and average device temperature $T_{dev}$. A full set of $I-V$ curves are obtained for various $T_{sub}$ values.

As is shown in Fig. 5, the measured $I-V$ for a $T_{sub}$ of 29 °C. The resulting device temperature is superimposed at each bias-point showing $T_{dev}$ exceeding 170 °C for high bias values. Also at high bias, the drain current is observed to decrease as a result of the self-heating in the device.
Fig. 5. Measured $I-V$, with $T_{\text{sub}}$ superimposed, for a constant substrate temperature of 29 °C.

Fig. 6. Predicted average device temperature (solid lines) compared with measured values (circles) using a single $R_{\text{th,eff}}$ for a given $T_{\text{sub}}$ of 29 °C.

Fig. 7. Tensor Product B-Splines (TPS) extracted (solid lines) and directly measured (circles) isothermal $I-V$ for $T_{\text{dev}} = 90$ °C with both substrate cooling and heating.

The large-signal electrothermal model for the LDMOSFET shown in Fig. 2, features a simple thermal network topology which calculates the steady state isothermal temperature of the LDMOSFET as a function of the power dissipated by the LDMOSFET.

An effective thermal resistance $R_{\text{th,eff}}$ (the sum of $R_{\text{th,k仪}}$ and $R_{\text{th,sub}}$), can be obtained by using a least squares fit on the temperature versus device power characteristics. A unique $R_{\text{th,eff}}$ value is extracted for each $T_{\text{sub}}$ and is found to be 9.26 °C/W for $T_{\text{sub}} = 29$ °C. At $T_{\text{sub}} = 89$ °C, $R_{\text{th,eff}}$ equals 8.74 °C/W. The effective thermal resistance is observed to be monotonously decreasing with increasing substrate temperature. Using this $R_{\text{th,eff}}$ value, we can compute the average device temperature for any bias. The solid lines in Fig. 6 show the predicted $T_{\text{dev}}$ for a $T_{\text{sub}}$ of 29 °C. The circles give the measured $T_{\text{dev}}$. Clearly, a single $R_{\text{th,eff}}$ (see [7] and [8]) can predict well the entire thermal map of the 1-mm$^2$ device tested despite its relatively large area. This also verifies the applicability of the thermal model used for defining the isothermal $I-V$ in (1).

III. EXTRACTION AND MEASUREMENT OF ISO-THERMAL $I-V$ CURVES

A. Numerical Extraction

Using three-dimensional (3-D) Tensor Product B-Splines (TPS) [9], [10], a function of three variables can be represented as

$$I_{\text{D,k仪}}(V_{\text{CS}}, V_{\text{DS}}, T_{\text{dev}}) = \sum_{i=1}^{m} \sum_{j=1}^{n} \sum_{k=1}^{p} \alpha_{ijk} B_{ijk, k, k, k}(V_{\text{CS}})B_{ijk, k, k, k}(V_{\text{DS}}) \times B_{ijk, k, k, k}(T_{\text{dev}}).$$

Using data from the complete dc and thermal characterization presented in Section II, the TPS method can be used to extract a complete set of isothermal $I-V$ characteristics for different average device temperatures. In Fig. 7, the TPS extracted isothermal $I-V$ for a $T_{\text{dev}}$ of 90 °C is given by the solid lines. The isothermal $I-V$ clearly do not contain the self-heating induced reduction of the drain current observed in the non isothermal $I-V$ curves at large drain voltages. The TPS method is limited by the range of the data available. Lowering the substrate temperature will allow for data at higher biases to be available for a given $T_{\text{dev}}$.

B. Direct Measurement

A novel approach to directly acquire isothermal $I-V$ characteristics and microwave data has been implemented in LabWindows. In this approach, the computer-controlled data-acquisition system maintains a constant device temperature $T_{\text{dev}}$ by acquiring $I-V$ and microwave data on constant power ($P_{\text{avg}}$) contours. In the measurement procedure, the substrate temperature is first set to the lowest temperature (in this case, cooled
to 18 °C) and \( V_{GS} \) is set to its highest value. \( V_{DS} \) is then swept and the drain current at all data points within ±2 °C of the targeted \( T_{dev} \) are recorded after establishing thermal equilibrium in the device (a 5 s pause was verified to be more than sufficient for a bias change with the same substrate temperature). \( V_{GS} \) is then lowered and the drain voltage sweep is repeated. Once the data has been acquired for the lowest \( V_{GS} \), the substrate temperature is increased each time (in this case by 4 °C with a 240 s delay allowed for the substrate to reach thermal equilibrium) and the \( V_{GS} \) and \( V_{DS} \) bias-sweep process is repeated. The higher the substrate temperature, the lower the drain voltages that will give the targeted device temperature \( T_{dev} \). This novel approach permits a rapid data acquisition since all data are acquired in a single sweep of the substrate temperature from its lowest to highest value. This procedure minimizes the impact of the thermal inertia of the substrate on the measurement time and is fully reproducible from measurement to measurement.

The circles in Fig. 7 show the directly measured 90 °C isothermal \( I-V \) characteristics, which is in excellent agreement with that extracted using TPS (solid lines). By cooling the substrate, the bias-range of the isothermal \( I-V \) acquired is increased since for a cooler substrate, the targeted \( T_{dev} \) is achieved for higher bias-voltages.

Finally, the \( T_{dev} \approx 75 °C \) pulsed \( I-V \) characteristics for two different (OFF and ON) dc bias-points are plotted in Fig. 8 together with the directly measured isothermal \( I-V \) characteristics. Pulses with a duration of 1 μs and 1% duty-rate are used. The ON and OFF pulsed \( I-V \) curves were shifted down by 10 mA to account for a difference in equipment calibration and enforce the required dc bias condition given by (4). A very good agreement is obtained between the isothermal and the ON pulsed \( I-V \) characteristics for all gate voltages. Note however, that a substantial difference is observed between the ON and OFF pulse \( I-V \) data, highlighting their dc bias dependence.

IV. EXTRACTION AND MEASUREMENT OF ISO-TERMAL \( S \)-PARAMETERS

The direct isothermal measurement method introduced in Section III can also be used for simultaneously measuring the microwave \( S \)-parameters (see Fig. 4) while acquiring the isothermal \( I-V \) characteristics. See [2] for examples of measured isothermal \( S \)-parameters acquired that way. The intrinsic \( \text{RF}_{gm} \) and \( \text{RF}_{gdt} \) were extracted from these \( S \)-parameter data using the analytic procedure described in [2].

It has been verified in [4] that for SOI-MOSFETs afflicted with a strong parasitic bipolar-transistor effect (see Fig. 3), the TPS integration of intrinsic \( \text{RF}_{gm} \) and \( \text{RF}_{gdt} \) with the dc boundary condition set by (4), yields the pulsed \( I-V \) characteristics for that dc bias-point and not the isothermal dc \( I-V \) characteristics. Therefore, to detect the presence of a low-frequency dispersion in LDMOSFET we compare in Fig. 9 for all biases, the transconductances extracted from the isothermal microwave \( S \)-parameters (RF\(_{gm}\)) and the isothermal \( I-V \) characteristics (\( \text{DC}_{gm} \)) which are measured at the same time. A good agreement is generally observed. This indicates that in these LDMOSFETs, the body tie suppresses the low-frequency dispersion effect associated with the parasitic bipolar-transistor. However, at large voltages a noticeable difference in \( \text{DC}_{gm} \) and \( \text{RF}_{gm} \) is observed. This is attributed to the increase of impact-ionization current which drives the parasitic bipolar-transistor.

V. CONCLUSION

We have presented in this paper two new approaches for the generation of isothermal dc and microwave characteristics of power RF LDMOSFETs. In the first approach, TPS representation was used to extract isothermal \( I-V \) data from dc \( I-V \) characteristics measured at various substrate temperatures. In the second approach, isothermal \( I-V \) and microwave
characteristics are directly measured with an efficient (constant power contour) experimental procedure that keeps the average device/gate temperature constant. An excellent agreement was demonstrated between the numerical extraction and the direct measurement approach for the $I-V$ characteristics. Finally, the correlation of the isothermal dc and microwave data acquired simultaneously with the direct measurement-technique, was analyzed.

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REFERENCES


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