

Voltage Equations in Arbitrary Reference -
Frame Variables

$$\bar{v}_{abc} = \bar{r}_s \dot{\lambda}_{abc} + p \lambda_{abc}$$

$$v'_{abc} = r'_r \dot{\lambda}'_{abc} + p \lambda'_{abc}$$

$$\lambda_{abc} = (\bar{L}_s) \dot{\lambda}_{abc} + [\bar{L}'_{sr}] \dot{\lambda}'_{abc}$$

$$\lambda'_{abc} = (\bar{L}'_{sr})^T \dot{\lambda}_{abc} + (\bar{L}'_r) \dot{\lambda}'_{abc}$$

$$\bar{v}_{abc} = K_s \bar{v}_{qdos} \quad \lambda_{abc} = K_s \bar{\lambda}_{qdos}$$

$$v'_{abc} = K_r \bar{v}'_{qdor} \quad \lambda'_{abc} = K_r \bar{\lambda}'_{qdor}$$

- using the above transformation equations, we can transform the voltage equations to an arbitrary reference frame rotating at speed of ω (see Fig 1)

$$v_{qdos} = r_s \dot{\lambda}_{qdos} + \omega \lambda_{dqs} + p \lambda_{qdos}$$

$$v'_{qdor} = r'_r \dot{\lambda}'_{qdor} + (\omega - \omega_r) \lambda'_{qdr} + p \lambda'_{qdor}$$

where

$$(\lambda_{qds})^T = [\lambda_{ds} \quad -\lambda_{qs} \quad 0]$$

$$(\lambda'_{qdr})^T = [\lambda'_{dr} \quad -\lambda'_{qr} \quad 0]$$

- Flux linkage equations in abc reference frame can be transformed to qd axes using K_s and K_r transformation matrices.

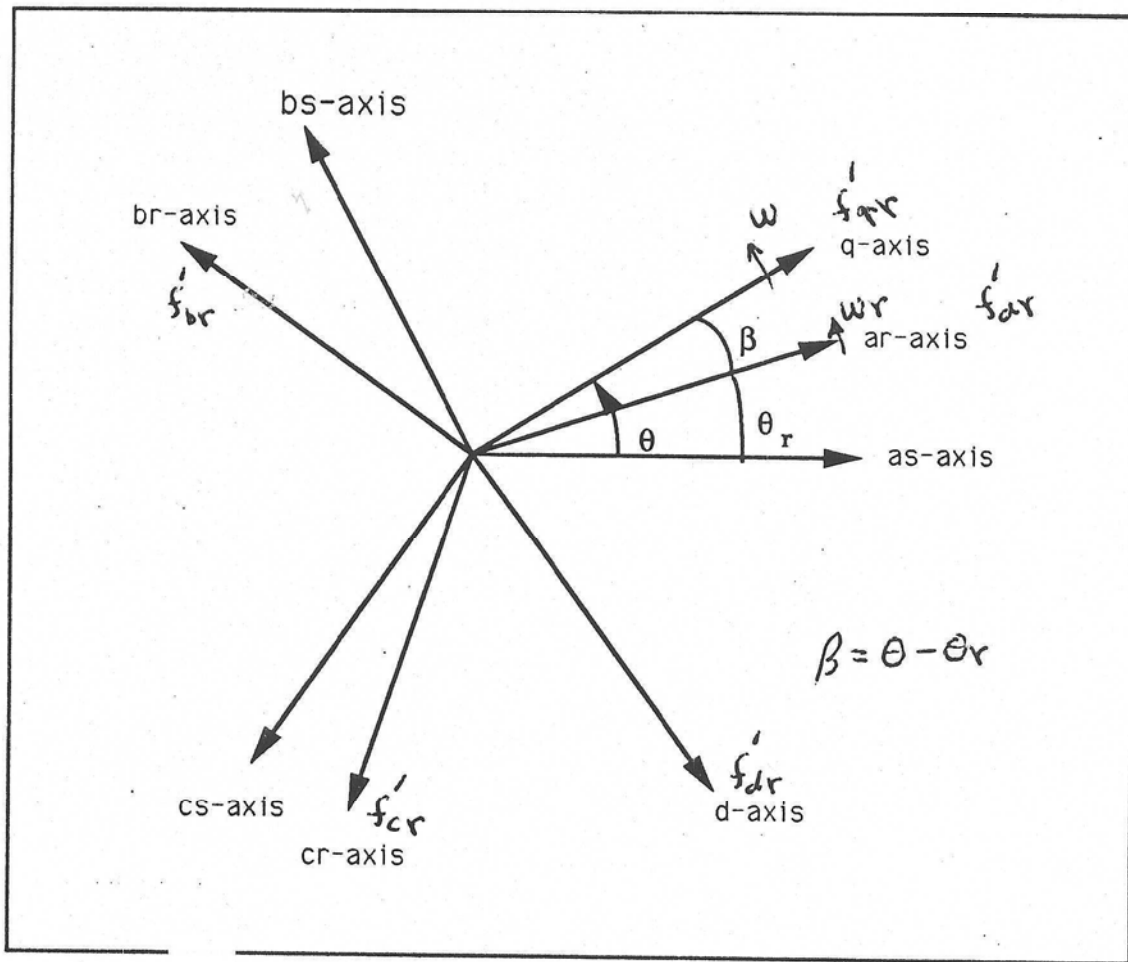


Fig 1 Axis of 2-pole, 3-phase symmetrical machine

$$\begin{bmatrix} \lambda_{qdos} \\ \lambda'_{qdor} \end{bmatrix} = \begin{bmatrix} K_s L_s (K_s)^{-1} & K_s L'_{sr} (K_r)^{-1} \\ K_r (L'_{sr}) (K_s)^{-1} & K_r L_r (K_r)^{-1} \end{bmatrix} \begin{bmatrix} \lambda_{qdos} \\ \lambda'_{qdor} \end{bmatrix}$$

where

$$K_s L_s (K_s)^{-1} = \begin{bmatrix} L_{ls} + M & 0 & 0 \\ 0 & L_{ls} + M & 0 \\ 0 & 0 & L_{ls} \end{bmatrix}$$

$$M = \frac{3}{2} L_{ms}$$

$$K_r L'_r (K_r)^{-1} = \begin{bmatrix} L'_{lr} + M & 0 & 0 \\ 0 & L'_{lr} + M & 0 \\ 0 & 0 & L'_{lr} \end{bmatrix}$$

And

$$K_s L'_{sr} (K_r)^{-1} = K_r (L'_{sr})^T (K_s)^{-1} = \begin{bmatrix} M & 0 & 0 \\ 0 & M & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

Voltage equations written in expanded form can be expressed as

$$v_{qs} = r_s i_{qs} + \omega \lambda_{ds} + p \lambda_{qs}$$

$$v_{ds} = r_s i_{ds} - \omega \lambda_{qs} + p \lambda_{ds}$$

$$v_{os} = r_s i_{os} + p \lambda_{os}$$

$$v'_{qr} = r'_r i'_{qr} + (\omega - \omega_r) \lambda'_{dr} + p \lambda'_{qr}$$

$$v'_{dr} = r'_r i'_{dr} - (\omega - \omega_r) \lambda'_{qr} + p \lambda'_{dr}$$

$$v'_{or} = r'_r i'_{or} + p \lambda'_{or}$$

Flux linkage equations are

$$\lambda_{qs} = L_{ls} \dot{\lambda}_{qs} + M(\dot{\lambda}_{qs} + \dot{\lambda}'_{qr})$$

$$\lambda_{ds} = L_{ls} \dot{\lambda}_{ds} + M(\dot{\lambda}_{ds} + \dot{\lambda}'_{dr})$$

$$\lambda_{os} = L_{ls} \dot{\lambda}_{os}$$

$$\lambda'_{qr} = L'_{lr} \dot{\lambda}'_{qr} + M(\dot{\lambda}_{qs} + \dot{\lambda}'_{qr})$$

$$\lambda'_{dr} = L'_{lr} \dot{\lambda}'_{dr} + M(\dot{\lambda}_{ds} + \dot{\lambda}'_{dr})$$

$$\lambda'_{or} = L'_{lr} \dot{\lambda}'_{or}$$

- since machine and power system parameters are nearly always given in ohms or percent or per unit of a base impedance, it is convenient to express the voltage and flux linkage equations in terms of reactances rather than inductances.

let

$$\psi = \lambda \omega_b$$

then

$$V_{qs} = r_s \dot{\lambda}_{qs} + \frac{\omega}{\omega_b} \psi_{ds} + \frac{p}{\omega_b} \psi_{qs}$$

$$V_{ds} = r_s \dot{\lambda}_{ds} - \frac{\omega}{\omega_b} \psi_{qs} + \frac{p}{\omega_b} \psi_{ds}$$

$$V_{os} = r_s \dot{\lambda}_{os} + \frac{p}{\omega_b} \psi_{os}$$

$$v'_{qr} = r'_r i'_{qr} + \frac{(\omega - \omega_r)}{\omega_b} \psi'_{dr} + \frac{p}{\omega_b} \psi'_{qr}$$

$$v'_{dr} = r'_r i'_{dr} - \frac{(\omega - \omega_r)}{\omega_b} \psi'_{qr} + \frac{p}{\omega_b} \psi'_{dr}$$

$$v'_{or} = r'_r i'_{or} + \frac{p}{\omega_b} \psi'_{or}$$

and flux linkages become flux linkages per second with the units of volts.

$$\psi_{qs} = X_{ls} i_{qs} + X_m (i_{qs} + i'_{qr})$$

$$\psi_{ds} = X_{ls} i_{ds} + X_m (i_{ds} + i'_{dr})$$

$$\psi_{os} = X_{ls} i_{os}$$

$$\psi'_{qr} = X'_{lr} i'_{qr} + X_m (i_{qs} + i'_{qr})$$

$$\psi'_{dr} = X'_{lr} i'_{dr} + X_m (i_{ds} + i'_{dr})$$

$$\psi'_{or} = X'_{lr} i'_{or}$$

- Fig. 2 presents the arbitrary reference-frame equivalent circuits for a three-phase symmetrical induction machine

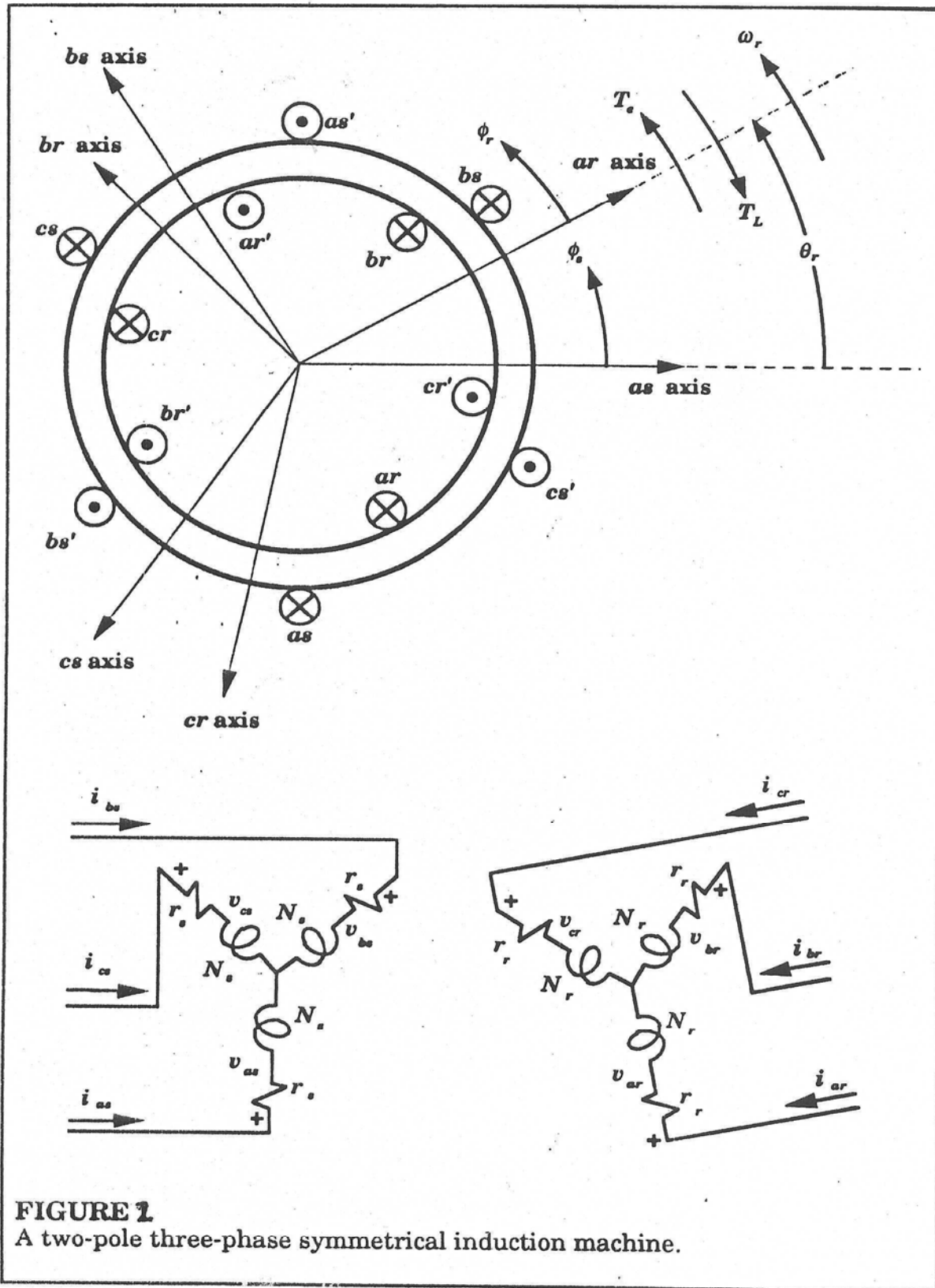


FIGURE 1
A two-pole three-phase symmetrical induction machine.

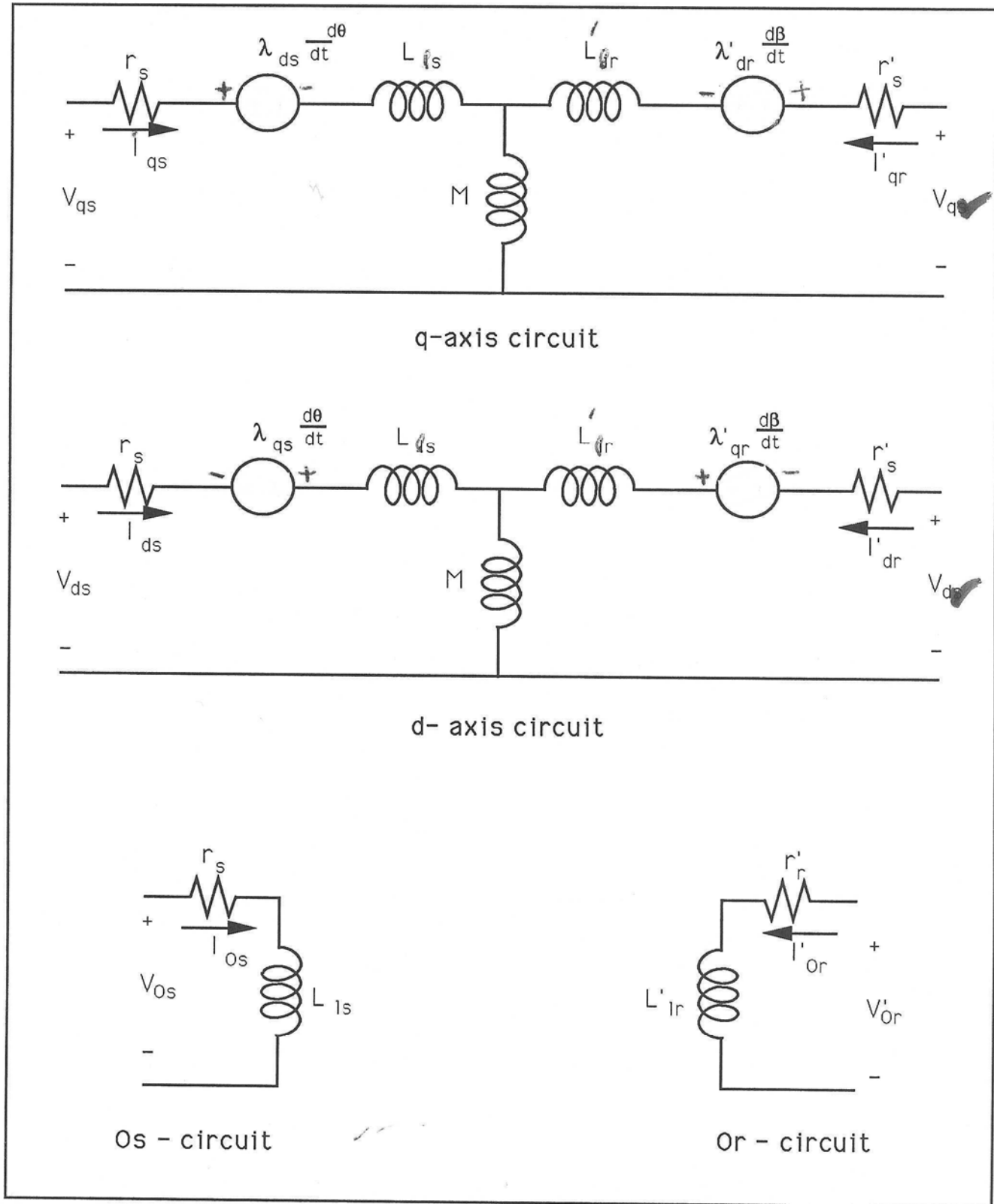


Fig. 3 Equivalent circuits of a 3-phase, symmetrical induction machine with rotating d-axis at speed of ω

Torque Equation in Arbitrary Reference - Frame Variables

- Electromagnetic torque in terms of arbitrary reference - frame variables may be obtained by substituting the equations of transformation in

$$T_e = \frac{P}{2} (i_{abc})^T \frac{d}{d\theta_r} (L'_{sr}) i'_{dbr}$$

$$T_e = \frac{P}{2} [(K_s)^{-1} i_{qdos}]^T \frac{d}{d\theta_r} [L'_{sr}] (K_r)^{-1} i'_{qdos}$$

After some work, we will have the following:

$$T_e = \left(\frac{3}{2}\right) \left(\frac{P}{2}\right) M (i_{qs} i'_{dr} - i_{ds} i'_{qr})$$

Where T_e is positive for motor action. Other expressions for the electromagnetic torque of an induction machine are

$$T_e = \left(\frac{3}{2}\right) \left(\frac{P}{2}\right) (i'_{qr} i'_{dr} - i'_{dr} i'_{qr})$$

$$T_e = \left(\frac{3}{2}\right) \left(\frac{P}{2}\right) (\lambda_{ds} i_{qs} - \lambda_{qs} i_{ds})$$

$$T_e = \frac{3}{2} \left(\frac{P}{2}\right) \left(\frac{1}{\omega_b}\right) (\psi'_{qr} i'_{dr} - \psi'_{dr} i'_{qr})$$