

- Winding arrangement for a 2-pole, 3 phase, wye-connected symmetrical induction machine is shown in Fig. 1. Stator windings are identical, sinusoidally distributed windings, displaced by 120° , with N_s equivalent turns and resistance r_s .
- Consider the case when rotor windings are also three identical sinusoidally distributed windings, displaced 120° , with N_r equivalent turns and resistance r_r .
- In abc reference frame, voltage equations can be written as

$$V_{abc} = r_s i_{abc} + P \lambda_{abc}$$

$$V_{abc} = r_r i_{abc} + P \lambda_{abc}$$

$$(f_{abc})^T = [f_{as} \quad f_{bs} \quad f_{cs}]$$

$$(f_{abc})^T = [f_{ar} \quad f_{br} \quad f_{cr}]$$

s: denotes variables and parameters associated with the stator circuits

r: denotes variables and parameters associated with the rotor circuits

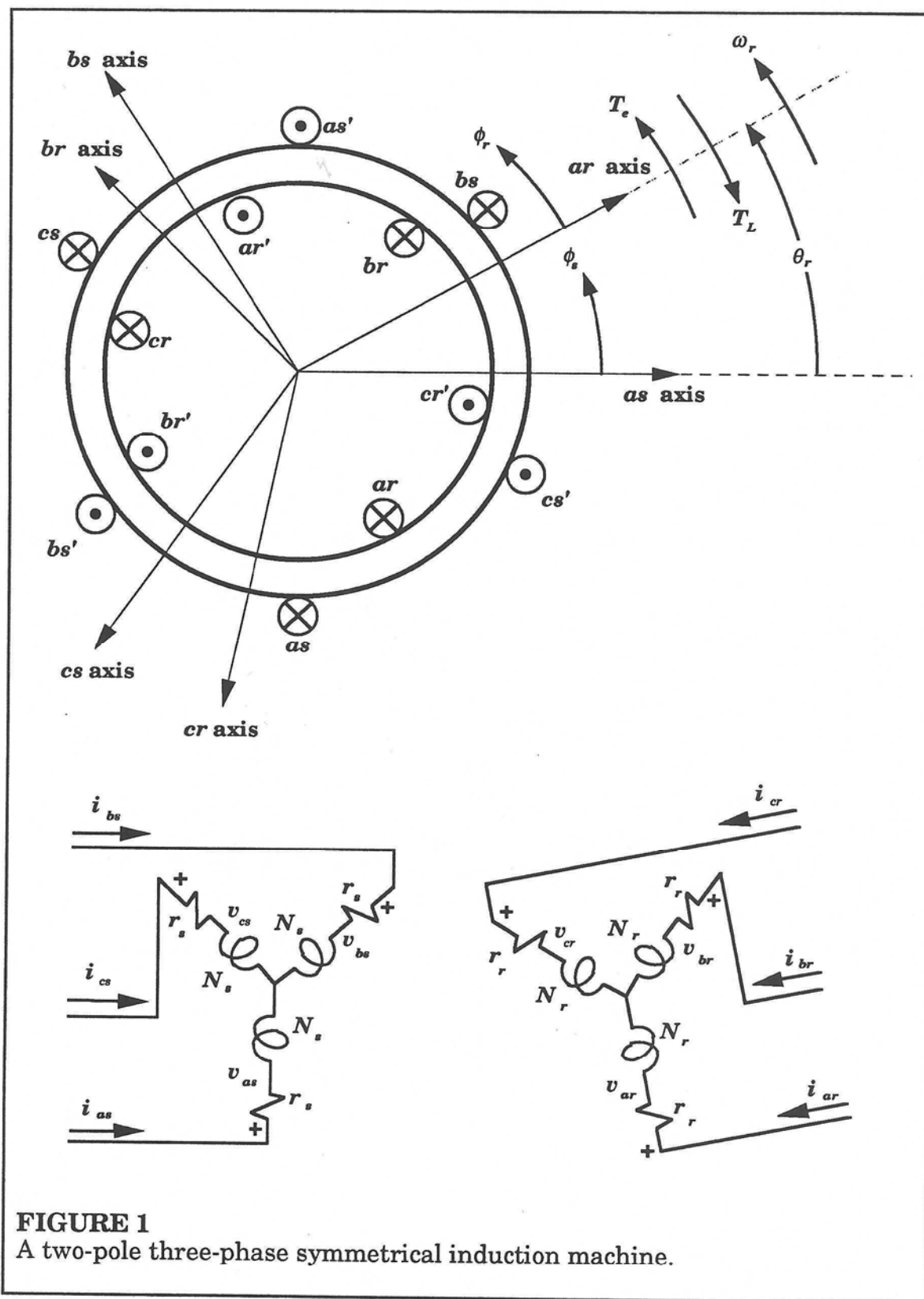


FIGURE 1
A two-pole three-phase symmetrical induction machine.

$$\begin{bmatrix} \lambda_{abcs} \\ \lambda_{abcr} \end{bmatrix} = \begin{bmatrix} L_s & L_{sr} \\ (L_{sr})^T & L_r \end{bmatrix} \begin{bmatrix} i_{abcs} \\ i_{abcr} \end{bmatrix}$$

where

$$L_s = \begin{bmatrix} L_{ls} + L_{ms} & -\frac{1}{2} L_{ms} & -\frac{1}{2} L_{ms} \\ -\frac{1}{2} L_{ms} & L_{ls} + L_{ms} & -\frac{1}{2} L_{ms} \\ -\frac{1}{2} L_{ms} & -\frac{1}{2} L_{ms} & L_{ls} + L_{ms} \end{bmatrix}$$

$$L_r = \begin{bmatrix} L_{lr} + L_{mr} & -\frac{1}{2} L_{mr} & -\frac{1}{2} L_{mr} \\ -\frac{1}{2} L_{mr} & L_{lr} + L_{mr} & -\frac{1}{2} L_{mr} \\ -\frac{1}{2} L_{mr} & -\frac{1}{2} L_{mr} & L_{lr} + L_{mr} \end{bmatrix}$$

$$L_{sr} = L_{sr} \begin{bmatrix} \cos \theta_r & \cos(\theta_r + \frac{2\pi}{3}) & \cos(\theta_r - \frac{2\pi}{3}) \\ \cos(\theta_r - \frac{2\pi}{3}) & \cos \theta_r & \cos(\theta_r + \frac{2\pi}{3}) \\ \cos(\theta_r + \frac{2\pi}{3}) & \cos(\theta_r - \frac{2\pi}{3}) & \cos \theta_r \end{bmatrix}$$

L_{ls} and L_{ms} are, respectively, the leakage and magnetising inductances of the stator windings

L_{lr} and L_{mr} are for the rotor winding (leakage and magnetising inductances)

' L_{sr} ': is the amplitude of the mutual inductances between stator and rotor windings

- A majority of induction machines are not equipped with coil-wound rotor windings; instead, the current flows in copper or aluminum bars which are uniformly distributed in a common ring at each end of the rotor. This type of rotor is referred to as a squirrel-cage rotor.

- Rotor variables can be referred to the stator windings by appropriate turns ratio.

$$i'_{abc r} = \frac{N_r}{N_s} i_{abc r}$$

$$v'_{abc r} = \frac{N_s}{N_r} v_{abc r}$$

$$\lambda'_{abc r} = \frac{N_s}{N_r} \lambda_{abc r}$$

$$L_{ms} = \frac{N_s}{N_r} L_{sr}$$

$$[L'_{sr}] = \frac{N_s}{N_r} [L_{sr}]$$

$$= L_{ms} \begin{bmatrix} \cos \theta_r & \cos(\theta_r + \frac{2\pi}{3}) & \cos(\theta_r - \frac{2\pi}{3}) \\ \cos(\theta_r - \frac{2\pi}{3}) & \cos \theta_r & \cos(\theta_r + \frac{2\pi}{3}) \\ \cos(\theta_r + \frac{2\pi}{3}) & \cos(\theta_r - \frac{2\pi}{3}) & \cos \theta_r \end{bmatrix}$$

Also,

$$L_{mr} = \left(\frac{N_r}{N_s}\right)^2 L_{ms}$$

$$[L'_r] = \left[\frac{N_r}{N_s}\right]^2 [L_r]$$

$$[L'_r] = \begin{bmatrix} L'_{er} + L_{ms} & -\frac{1}{2} L_{ms} & -\frac{1}{2} L_{ms} \\ -\frac{1}{2} L_{ms} & L'_{er} + L_{ms} & -\frac{1}{2} L_{ms} \\ -\frac{1}{2} L_{ms} & -\frac{1}{2} L_{ms} & L'_{er} + L_{ms} \end{bmatrix}$$

where

$$L'_{er} = \left(\frac{N_s}{N_r}\right)^2 L_{er}$$

Flux linkages may be expressed as

$$\begin{bmatrix} \lambda_{abcs} \\ \lambda'_{abcr} \end{bmatrix} = \begin{bmatrix} L_s & L'_{sr} \\ (L'_{sr})^T & L'_r \end{bmatrix} \begin{bmatrix} i_{abcs} \\ i'_{abcr} \end{bmatrix}$$

Voltage equations expressed in terms of machine variables referred to the stator windings may be written as

$$\begin{bmatrix} V_{abcs} \\ V'_{abcr} \end{bmatrix} = \begin{bmatrix} R_s + pL_s & pL'_{sr} \\ p(L'_{sr})^T & R'_r + pL'_r \end{bmatrix} \begin{bmatrix} i_{abcs} \\ i'_{abcr} \end{bmatrix}$$

where

$$R'_r = \left(\frac{N_s}{N_r}\right)^2 R_r$$

Torque Equation in Machine Variables

- Energy stored in the coupling field may be written as

$$W_c = W_f = \frac{1}{2} (\dot{\lambda}_{abcs})^T (\mathbf{L}_s - L_{fs} \mathbf{I}) \dot{\lambda}_{abcs} + (\dot{\lambda}_{abcs})^T \mathbf{L}'_{sr} \dot{\lambda}'_{abcr} + \frac{1}{2} (\dot{\lambda}'_{abcr})^T (\mathbf{L}'_r - L'_{er} \mathbf{I}) \dot{\lambda}'_{abcr}$$

\mathbf{I} : an identity matrix

$$T_e(\dot{\lambda}_j, \theta_r) = \frac{P}{2} \frac{\partial W_c(\dot{\lambda}_j, \theta_r)}{\partial \theta_r}$$

- since \mathbf{L}_s and \mathbf{L}'_r are functions of θ_r , the above equation for the electromagnetic torque yields.

$$T_e = \left(\frac{P}{2}\right) (\dot{\lambda}_{abcs})^T \frac{\partial}{\partial \theta_r} [\mathbf{L}'_{sr}] \dot{\lambda}'_{abcr}$$

or

$$T_e = -\left(\frac{P}{2}\right) L_{ms} \left\{ \dot{\lambda}_{as} (\dot{\lambda}'_{ar} - \frac{1}{2} \dot{\lambda}'_{br} - \frac{1}{2} \dot{\lambda}'_{cr}) + \dot{\lambda}_{bs} (\dot{\lambda}'_{br} - \frac{1}{2} \dot{\lambda}'_{ar} - \frac{1}{2} \dot{\lambda}'_{cr}) + \dot{\lambda}_{cs} (\dot{\lambda}'_{cr} - \frac{1}{2} \dot{\lambda}'_{br} - \frac{1}{2} \dot{\lambda}'_{ar}) \right\} \sin \theta_r + \frac{\sqrt{3}}{2} \left[\dot{\lambda}_{as} (\dot{\lambda}'_{br} - \dot{\lambda}'_{cr}) + \dot{\lambda}_{bs} (\dot{\lambda}'_{cr} - \dot{\lambda}'_{ar}) + \dot{\lambda}_{cs} (\dot{\lambda}'_{ar} - \dot{\lambda}'_{br}) \right] \cos \theta_r$$

The torque and rotor speed are related by

$$T_e = \mathcal{J} \left(\frac{2}{p}\right) P \omega_r + T_L$$

Equations of Transformation for Rotor Circuits.

- In the analysis of induction machines it is desirable to transform the variables associated with the symmetrical rotor windings to the arbitrary reference frame.

$$f'_{qdor} = K_r f'_{abcr}$$

$$(f'_{qdor})^T = [f'_{ar} \ f'_{br} \ f'_{or}]$$

$$(f'_{abcr})^T = [f'_{ar} \ f'_{br} \ f'_{or}]$$

$$K_r = \frac{2}{3} \begin{bmatrix} \cos \beta & \cos(\beta - \frac{2\pi}{3}) & \cos(\beta + \frac{2\pi}{3}) \\ \sin \beta & \sin(\beta - \frac{2\pi}{3}) & \sin(\beta + \frac{2\pi}{3}) \\ \frac{1}{2} & \frac{1}{2} & \frac{1}{2} \end{bmatrix}$$

where $\beta = \theta - \theta_r$ (see Fig. 2)

$$\theta_r = \int_0^t \omega_r(\tau) d\tau + \theta_r(0)$$

$$(K_r)^{-1} = \begin{bmatrix} \cos \beta & -\sin \beta & 1 \\ \cos(\beta - \frac{2\pi}{3}) & \sin(\beta - \frac{2\pi}{3}) & 1 \\ \cos(\beta + \frac{2\pi}{3}) & \sin(\beta + \frac{2\pi}{3}) & 1 \end{bmatrix}$$

'r' subscript indicates the variables, parameters and transformation associated with rotating circuits

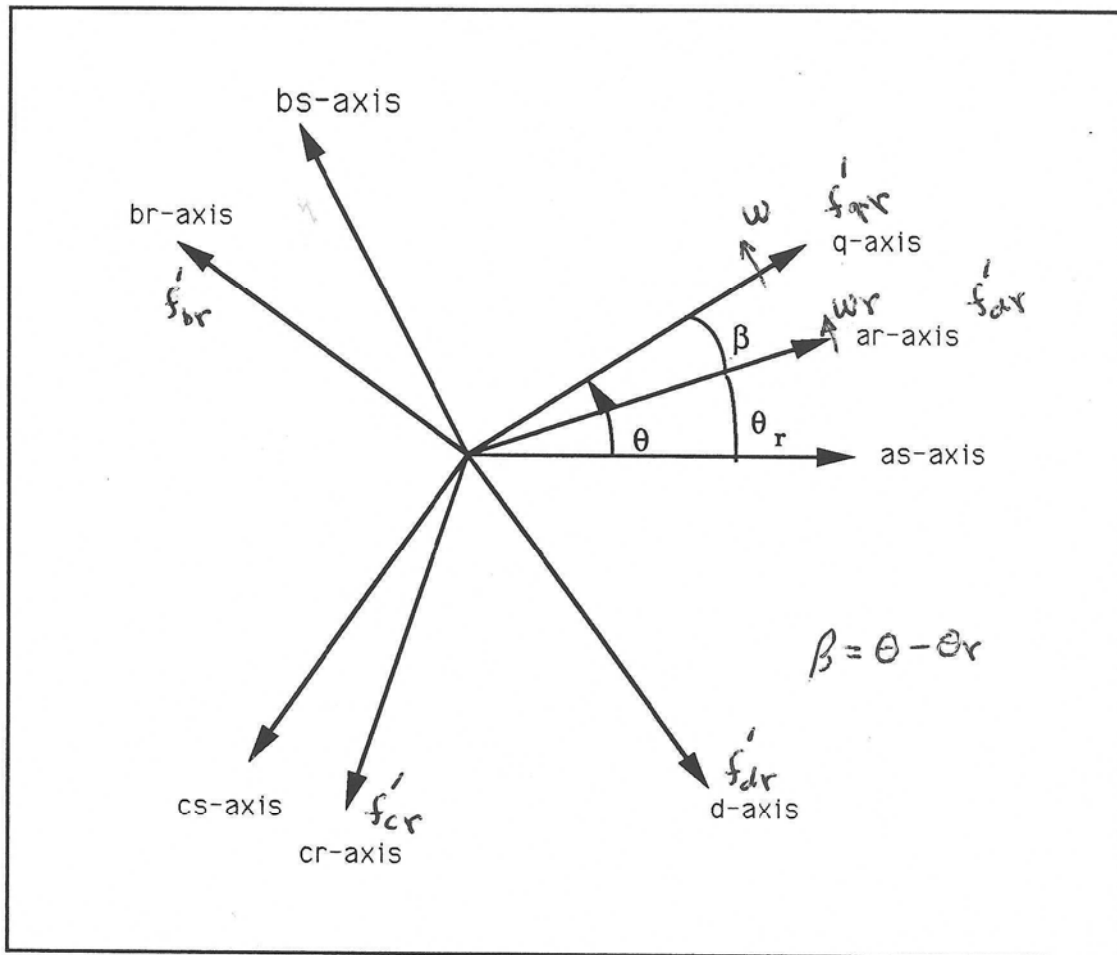


Fig. 2 Axis of 2-pole, 3-phase symmetrical machine